

**A NEW APPROACH TO THE PERTURBATION ANALYSIS  
FOR DISCRETE  $\mathcal{H}_\infty$  SYNTHESIS PROBLEMS\***

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The paper presents a new approach for obtaining local linear perturbation bounds for the discrete  $\mathcal{H}_\infty$  synthesis problem based on linear matrix inequalities (LMI). The sensitivity analysis of the perturbed LMI is done by introducing a suitable slightly perturbed right-hand part. This approach leads to tight local linear perturbation bounds for the LMI solutions of the  $\mathcal{H}_\infty$  synthesis problem. Numerical example illustrating the theoretical results is presented.

**1. Introduction.** In many control problems the design constraints have a simple reformulation in terms of linear matrix inequalities (LMI) [1, 6]. The  $\mathcal{H}_\infty$  control problem is an example of this in this field. Indeed, the  $\mathcal{H}_\infty$  constraints can be expressed as a single matrix inequality *via* the bounded real lemma [4]. It must be stressed that the  $\mathcal{H}_\infty$  control problem has a solution in terms of Riccati equations [7], the LMI approach remains valuable.

In this paper we propose a new approach to the local sensitivity analysis of the LMI based  $\mathcal{H}_\infty$  synthesis problem by introducing a suitable right-hand part in the corresponding matrix inequalities.

The paper is organized as follows. In Section 2 we shortly present the problem setup and objective. Section 3 describes the performed local linear sensitivity analysis of the LMI based  $\mathcal{H}_\infty$  synthesis problem. Section 4 presents a numerical example. Section 5 contains some final remarks.

**2. Problem Statement.** Consider the discrete-time autonomous linear control system

$$(1) \quad \begin{aligned} x_{k+1} &= Ax_k + B_1 w_k + B_2 u_k, \\ z_k &= C_1 x_k + D_{11} w_k + D_{12} u_k, \\ y_k &= C_2 x_k + D_{21} w_k + D_{22} u_k, \end{aligned}$$

where  $x_k \in \mathbb{R}^n$  is the state vector,  $w_k \in \mathbb{R}^l$  is the exogenous input vector,  $u_k \in \mathbb{R}^m$  is the control input vector,  $z_k \in \mathbb{R}^p$  is the error vector,  $y_k \in \mathbb{R}^r$  is the measurement vector and  $A, B_1, B_2, C_1, C_2, D_{11}, D_{12}, D_{21}, D_{22}$  are constant matrices of compatible size.

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The formulation and solution of corresponding  $\mathcal{H}_\infty$  control problems are well-known, see e.g. [7].

We consider an LMI approach to solve the  $\mathcal{H}_\infty$  synthesis problem, as stated in [2]. More precisely, we are interested in the solution of the LMI [2, 6]

$$(2) \quad \begin{bmatrix} \mathcal{N}_{12} & \vdots & 0 \\ \dots & \dots & \dots \\ 0 & \vdots & I \end{bmatrix}^\top \begin{bmatrix} ARA^\top - R & ARC_1^\top & \vdots & B_1 \\ C_1RA^\top & -\gamma I + C_1RC_1^\top & \vdots & D_{11} \\ \dots & \dots & \dots & \dots \\ B_1^\top & D_{11}^\top & \vdots & -\gamma I \end{bmatrix} \begin{bmatrix} \mathcal{N}_{12} & \vdots & 0 \\ \dots & \dots & \dots \\ 0 & \vdots & I \end{bmatrix} < 0,$$

$$(3) \quad \begin{bmatrix} \mathcal{N}_{21} & \vdots & 0 \\ \dots & \dots & \dots \\ 0 & \vdots & I \end{bmatrix}^\top \begin{bmatrix} A^\top SA - S & A^\top SB_1 & \vdots & C_1^\top \\ B_1^\top SA & -\gamma I + B_1^\top SB_1 & \vdots & D_{11}^\top \\ \dots & \dots & \dots & \dots \\ C_1 & D_{11} & \vdots & -\gamma I \end{bmatrix} \begin{bmatrix} \mathcal{N}_{21} & \vdots & 0 \\ \dots & \dots & \dots \\ 0 & \vdots & I \end{bmatrix} < 0,$$

$$(4) \quad \begin{bmatrix} R & I \\ I & S \end{bmatrix} > 0,$$

where  $\mathcal{N}_{12}$  and  $\mathcal{N}_{21}$  are the orthonormal bases of the null-spaces of  $[B_2^\top D_{12}^\top]$  and  $[C_2 D_{21}]$ , respectively. Here we assume that the optimal closed-loop performance  $\gamma_{\text{opt}}$  of the system (1) is already obtained.

The main objective point of the paper is to perform a local linear sensitivity analysis of the LMI system (2)–(3) near the optimal value of  $\gamma$ .

Suppose that the matrices  $A, B_1, B_2, C_1, C_2, D_{11}, D_{12}, D_{21}, D_{22}$  are subject to perturbations  $\Delta A, \Delta B_1, \Delta B_2, \Delta C_1, \Delta C_2, \Delta D_{11}, \Delta D_{12}, \Delta D_{21}, \Delta D_{22}$  and assume that these perturbations do not change the sign of the LMI (2)–(3).

**3. Linear Sensitivity Analysis.** First, we perform a sensitivity analysis of the LMI (3). The structure of this LMI allows to consider only the part

$$(5) \quad \begin{aligned} & (\mathcal{N}_{21} + \Delta\mathcal{N}_{21})^\top \\ & * \left\{ \begin{bmatrix} (A + \Delta A)^\top (S^* + \Delta S)(A + \Delta A) - (S^* + \Delta S) & 0 \\ (B_1 + \Delta B_1)^\top (S^* + \Delta S)(A + \Delta A) & 0 \end{bmatrix} \right. \\ & \left. + \begin{bmatrix} 0 & (A + \Delta A)^\top (S^* + \Delta S)(B_1 + \Delta B_1) \\ 0 & -\gamma_{\text{opt}} I - \Delta\gamma_{\text{opt}} I + (B_1 + \Delta B_1)^\top (S + \Delta S)(B_1 + \Delta B_1) \end{bmatrix} \right\} \\ & * (\mathcal{N}_{21} + \Delta\mathcal{N}_{21}) = \bar{\mathcal{H}}^* + \Delta\bar{\mathcal{H}}_1 < 0, \end{aligned}$$

and to study the effect of the perturbations  $\Delta A, \Delta B_1, \Delta B_2, \Delta C_1, \Delta C_2, \Delta D_{11}, \Delta D_{12}, \Delta D_{21}, \Delta D_{22}$  and  $\Delta\gamma_{\text{opt}}$  on the perturbed LMI solution  $S^* + \Delta S$ , where  $S^*$  and  $\Delta S$  are the nominal solution of LMI (3) and the perturbation. The essence of our approach is to perform sensitivity analysis of the LMI (3) in a similar manner as for a proper matrix equation after introducing a suitable right-hand part, which is slightly perturbed. The matrix  $\bar{\mathcal{H}}^*$  is obtained using the nominal LMI

$$(6) \quad \mathcal{N}_{21}^\top \begin{bmatrix} A^\top S^* A - S^* & A^\top S^* B_1 \\ B_1^\top S^* A & -\gamma_{\text{opt}} I + B_1^\top S^* B_1 \end{bmatrix} \mathcal{N}_{21} = \bar{\mathcal{H}}^* < 0.$$

The matrix  $\bar{\mathcal{H}}_1$  is due to the data and closed-loop performance perturbations, the rounding errors during the numerical solution and the sensitivity of the interior-point method used to solve the LMI. It is important to mention that the (1,2), (2,1), (2,2) blocks of the LMI (2) and (3) pose constraints on the size of the perturbations  $\Delta B_1$ ,  $\Delta C_1$ ,  $\Delta D_{11}$  and  $\Delta \gamma_{\text{opt}}$ , since the introduced right-hand part matrix must be negatively definite.

The perturbed relation (5) may be written as

$$(7) \quad \mathcal{N}_{21}^\top \bar{\mathcal{V}} \mathcal{N}_{21} + \mathcal{N}_{21}^\top \bar{\mathcal{V}} \Delta \mathcal{N}_{21} + \Delta \mathcal{N}_{21}^\top \bar{\mathcal{V}} \mathcal{N}_{21} + \Delta \mathcal{N}_{21}^\top \bar{\mathcal{V}} \Delta \mathcal{N}_{21} = \bar{\mathcal{H}}^* + \Delta \bar{\mathcal{H}}_1,$$

where

$$\bar{\mathcal{V}} = \begin{bmatrix} A^\top S^* A - S^* + A^\top \Delta S A - \Delta S + A^\top S^* \Delta A + \Delta A^\top S^* A & 0 \\ B_1^\top S^* A + B_1 \Delta S A + B_1^\top S^* \Delta A + \Delta B_1^\top S^* A & 0 \end{bmatrix} \\ + \begin{bmatrix} 0 & A^\top S^* B_1 + A^\top \Delta S B_1 + A^\top S^* \Delta B_1 + \Delta A^\top S^* B_1 \\ 0 & -\gamma_{\text{opt}} I - \Delta \gamma_{\text{opt}} I + B_1^\top S^* B_1 + B_1^\top \Delta S^* B_1 + B_1^\top S^* \Delta B_1 + \Delta B_1^\top S^* B_1 \end{bmatrix}.$$

Here the terms of second and higher order are neglected. Next, we use relation (6) to obtain the expression

$$(8) \quad \mathcal{N}_{21}^\top \Psi_S \mathcal{N}_{21} + \mathcal{N}_{21}^\top (\mathcal{H}^* + \Psi_S) \Delta \mathcal{N}_{21} + \Delta \mathcal{N}_{21}^\top (\mathcal{H}^* + \Psi_S) \mathcal{N}_{21} + \Delta \mathcal{N}_{21}^\top (\mathcal{H}^* + \Psi_S) \Delta \mathcal{N}_{21} = \Delta \bar{\mathcal{H}}_1,$$

where

$$\bar{\mathcal{H}}^* = \mathcal{N}_{21}^\top \mathcal{H}^* \mathcal{N}_{21}, \quad \Psi_S = \Theta_S + \Lambda_S, \quad \Theta_S = \begin{bmatrix} A^\top \Delta S A - \Delta S & A^\top \Delta S B_1 \\ B_1^\top \Delta S A & B_1^\top \Delta S B_1 \end{bmatrix}, \\ \Lambda_S = \begin{bmatrix} A^\top S^* \Delta A + \Delta A^\top S^* A & A^\top S^* \Delta B_1 + \Delta A^\top S^* B_1 \\ B_1^\top S^* \Delta A + \Delta B_1^\top S^* A & B_1^\top S^* \Delta B_1 + \Delta B_1^\top S^* B_1 - \Delta \gamma_{\text{opt}} I \end{bmatrix}.$$

Since we are going to obtain linear perturbation bounds for the LMI based  $\mathcal{H}_\infty$  synthesis problem, the terms of second and higher order in (8) will be neglected. Hence, (8) yields

$$(9) \quad \mathcal{N}_{21}^\top \Theta_S \mathcal{N}_{21} + \mathcal{N}_{21}^\top \Lambda_S \mathcal{N}_{21} + \Delta \mathcal{N}_{21}^\top \mathcal{H}^* \mathcal{N}_{21} + \mathcal{N}_{21}^\top \mathcal{H}^* \Delta \mathcal{N}_{21} = \Delta \bar{\mathcal{H}}_1.$$

We use the setting  $\mathcal{H}^* \mathcal{N}_{21} = \tilde{\mathcal{N}}_{21}$ ,  $\mathcal{N}_{21}^\top \mathcal{H}^* = \tilde{\mathcal{N}}_{21}^*$ ,  $A^\top S^* = S_{A^\top}^*$ ,  $S^* A = S_A^*$ ,  $B_1^\top S^* = S_{B_1^\top}^*$ ,  $S^* B_1 = S_{B_1}^*$ . In this way relation (9) may be written in a vector form as

$$(10) \quad (\mathcal{N}_{21}^\top \otimes \mathcal{N}_{21}^\top) \text{vec}(\Theta_S) + (\mathcal{N}_{21}^\top \otimes \mathcal{N}_{21}^\top) \text{vec}(\Lambda_S) + \mathcal{N}_{S\Theta} \text{vec}(\Delta \mathcal{N}_{21}) = \text{vec}(\Delta \bar{\mathcal{H}}_1),$$

where

$$\text{vec}(\Theta_S) = \begin{bmatrix} A^\top \otimes A^\top - I_{n^2} \\ B_1^\top \otimes A^\top \\ A^\top \otimes B_1^\top \\ B_1^\top \otimes B_1^\top \end{bmatrix} \text{vec}(\Delta S) = N \Delta S, \\ \text{vec}(\Lambda_S) = \begin{bmatrix} (I \otimes S_{A^\top}^*) + (S_A^* \otimes I) \Pi_{n^2} & 0 & 0 \\ (S_{B_1}^* \otimes I) \Pi_{n^2} & (I \otimes S_{A^\top}^*) & 0 \\ (I \otimes S_{B_1^\top}^*) & (S_A^* \otimes I) \Pi_{l^2} & 0 \\ 0 & (I \otimes S_{B_1^\top}^*) + (S_{B_1}^* \otimes I) \Pi_{l^2} & -e_{l^3} \end{bmatrix} \begin{bmatrix} \text{vec}(\Delta A) \\ \text{vec}(\Delta B_1) \\ \Delta \gamma_{\text{opt}} \end{bmatrix} \\ = [N_{t1} \ N_{t2} \ N_{t3}] \Delta \gamma_{ab1} = N_t \Delta \gamma_{ab1}, \quad \mathcal{N}_{S\Theta} = (\tilde{\mathcal{N}}_{21}^\top \otimes I) \Pi_{(n+l), n^2} + (I \otimes \tilde{\mathcal{N}}_{21}^*{}^\top).$$

Further, we obtain the expression

$$(11) \quad N_s \Delta s + N_{ts1} \text{vec}(\Delta A) + N_{ts2} \text{vec}(\Delta B_1) + N_{ts3} \Delta \gamma + \mathcal{N}_{S\Theta} \text{vec}(\Delta \mathcal{N}_{21}) = \text{vec}(\Delta \bar{\mathcal{H}}_1),$$

where

$$\begin{aligned} N_s &= (\mathcal{N}_{21}^\top \otimes \mathcal{N}_{21}^\top) N, \quad N_{ts1} = (\mathcal{N}_{21}^\top \otimes \mathcal{N}_{21}^\top) N_{t1}, \\ N_{ts2} &= (\mathcal{N}_{21}^\top \otimes \mathcal{N}_{21}^\top) N_{t2}, \quad N_{ts3} = (\mathcal{N}_{21}^\top \otimes \mathcal{N}_{21}^\top) N_{t3}. \end{aligned}$$

It is well-known [5] that the perturbation bound for the projector  $\mathcal{N}_{21}$  may be written as

$$(12) \quad \|\Delta \mathcal{N}_{21}\|_2 \leq \| [C_2, D_{21}]^\dagger \|_2 \| [\Delta C_2, \Delta D_{21}] \|_2.$$

Using also the fact that  $\|\text{vec}(M)\|_2 = \|M\|_{\mathcal{F}}$ , we can finally obtain that the relative perturbation bound for the solution  $S^*$  of the LMI (3) has the form

$$(13) \quad \begin{aligned} \frac{\|\Delta s\|_2}{\|S^*\|_{\mathcal{F}}} &\leq \frac{1}{\|S^*\|_{\mathcal{F}}} \left( N_{ab1} \frac{\|\Delta A\|_{\mathcal{F}}}{\|A\|_{\mathcal{F}}} + N_{ab2} \frac{\|\Delta B_1\|_{\mathcal{F}}}{\|B_1\|_{\mathcal{F}}} + N_{ab3} \frac{|\Delta \gamma_{\text{opt}}|}{|\gamma_{\text{opt}}|} \right) \\ &+ \frac{1}{\|S^*\|_{\mathcal{F}}} \left( N_{cd} \frac{\|[\Delta C_2, \Delta D_{21}]\|_{\mathcal{F}}}{\|[C_2, D_{21}]\|_{\mathcal{F}}} + N_1 \frac{\|\Delta \bar{\mathcal{H}}_1\|_{\mathcal{F}}}{\|\bar{\mathcal{H}}^*\|_{\mathcal{F}}} \right), \end{aligned}$$

where

$$\begin{aligned} \frac{N_{ab1}}{\|S^*\|_{\mathcal{F}}} &= \frac{\|N_s^\dagger\|_2 \|N_{ts1}\|_2 \|A\|_{\mathcal{F}}}{\|S^*\|_{\mathcal{F}}}, \quad \frac{N_{ab2}}{\|S^*\|_{\mathcal{F}}} = \frac{\|N_s^\dagger\|_2 \|N_{ts2}\|_2 \|\text{vec}(B_1)\|_2}{\|S^*\|_{\mathcal{F}}}, \\ \frac{N_{ab3}}{\|S^*\|_{\mathcal{F}}} &= \frac{\|N_s^\dagger\|_2 \|N_{ts3}\|_2 |\gamma|}{\|S^*\|_{\mathcal{F}}}, \quad \frac{N_1}{\|S^*\|_{\mathcal{F}}} = \frac{\|N_s^\dagger\|_2 \|\bar{\mathcal{H}}^*\|_{\mathcal{F}}}{\|S^*\|_{\mathcal{F}}} \\ \frac{N_{cd}}{\|S^*\|_{\mathcal{F}}} &= \frac{\|N_s^\dagger\|_2 \|\mathcal{N}_{S\Theta}\|_2 \| [C_2, D_{21}]^\dagger \|_{\mathcal{F}} \| [C_2, D_{21}] \|_{\mathcal{F}}}{\|S^*\|_{\mathcal{F}}}, \end{aligned}$$

may be considered as individual relative condition numbers of the LMI (3) with respect to the perturbations  $\Delta A$ ,  $\Delta B_1$ ,  $\Delta B_2$ ,  $\Delta C_1$ ,  $\Delta C_2$ ,  $\Delta D_{11}$ ,  $\Delta D_{12}$ ,  $\Delta D_{21}$  and  $\Delta \gamma_{\text{opt}}$ .

In a similar way the relative perturbation bounds for the solution  $R^*$  of the LMI (2) may be obtained using the expression

$$(14) \quad \begin{aligned} \frac{\|\Delta r\|_2}{\|R^*\|_{\mathcal{F}}} &\leq \frac{1}{\|R^*\|_{\mathcal{F}}} \left( M_{ac1} \frac{\|\Delta A\|_{\mathcal{F}}}{\|A\|_{\mathcal{F}}} + M_{ac2} \frac{\|\Delta C_1\|_{\mathcal{F}}}{\|C_1\|_{\mathcal{F}}} + \|M_{ac3}\|_2 \frac{|\Delta \gamma_{\text{opt}}|}{|\gamma_{\text{opt}}|} \right) \\ &+ \frac{1}{\|R^*\|_{\mathcal{F}}} \left( M_{bd} \frac{\|[\Delta B_2^\top, \Delta D_{12}^\top]\|_{\mathcal{F}}}{\|[B_2^\top, D_{12}^\top]\|_{\mathcal{F}}} + M_1 \frac{\|\Delta \bar{\mathcal{E}}_1\|_{\mathcal{F}}}{\|\bar{\mathcal{E}}^*\|_{\mathcal{F}}} \right), \end{aligned}$$

where  $\frac{M_{ac1}}{\|R^*\|_{\mathcal{F}}}$ ,  $\frac{M_{ac2}}{\|R^*\|_{\mathcal{F}}}$ ,  $\frac{M_{ac3}}{\|R^*\|_{\mathcal{F}}}$ ,  $\frac{M_1}{\|R^*\|_{\mathcal{F}}}$  and  $\frac{M_{bd}}{\|R^*\|_{\mathcal{F}}}$  may be considered as individual relative condition numbers of the LMI (2) with respect to the perturbations  $\Delta A$ ,  $\Delta B_1$ ,  $\Delta B_2$ ,  $\Delta C_1$ ,  $\Delta C_2$ ,  $\Delta D_{11}$ ,  $\Delta D_{12}$ ,  $\Delta D_{21}$  and  $\Delta \gamma_{\text{opt}}$ . These condition numbers can be obtained in a similar way to  $\frac{N_{ab1}}{\|S^*\|_{\mathcal{F}}}$ ,  $\frac{N_{ab2}}{\|S^*\|_{\mathcal{F}}}$ ,  $\frac{N_{ab3}}{\|S^*\|_{\mathcal{F}}}$ ,  $\frac{N_1}{\|S^*\|_{\mathcal{F}}}$  and  $\frac{N_{cd}}{\|S^*\|_{\mathcal{F}}}$ .

**4. Numerical Example.** Consider the following system description

$$A_c = \begin{bmatrix} 0 & 1 \\ -k/m & -c/m \end{bmatrix}, \quad B_{1c} = \begin{bmatrix} 0 & 0 & 0 \\ -pm & -pc/m & -pk/m \end{bmatrix}, \quad B_{2c} = \begin{bmatrix} 0 \\ 1/m \end{bmatrix},$$

$$C_{1c} = \begin{bmatrix} -k/m & -c/m \\ 0 & c \\ k & 0 \end{bmatrix}, C_{2c} = [1 \ 0], D_{11c} = \begin{bmatrix} -pm & -pc/m & -pk/m \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix},$$

$$D_{12c} = \begin{bmatrix} 1/m \\ 0 \\ 0 \end{bmatrix}, D_{21c} = [0 \ 0 \ 0]$$

and  $m = 3$ ,  $c = 1$ ,  $k = 2$ ,  $pm = 0.4$ ,  $pc = 0.2$ ,  $pk = 0.3$ . Here  $A_c$ ,  $B_{1c}$ ,  $B_{2c}$ ,  $C_{1c}$ ,  $C_{2c}$ ,  $D_{11c}$ ,  $D_{12c}$ ,  $D_{21c}$  are the system matrices of a continuous-time system, which for the aim of the analysis is turned into a discrete one using sampling time of 0.01s.

The perturbations in the system matrices of the system are chosen as

$$\Delta A = A \times 10^{-i}, \Delta B_1 = B_1 \times 10^{-i}, \Delta B_2 = B_2 \times 10^{-i},$$

$$\Delta C_1 = C_1 \times 10^{-i}, \Delta C_2 = C_2 \times 10^{-i}, \Delta D_{11} = D_{11} \times 10^{-i}, \Delta D_{12} = D_{12} \times 10^{-i},$$

$$\Delta \gamma_{\text{opt}} = 10^{-i} * \gamma_{\text{opt}}, \Delta \bar{\mathcal{H}}_1 = 10^{-i} * \bar{\mathcal{H}}^*, \Delta \bar{\mathcal{E}}_1 = 10^{-i} * \bar{\mathcal{E}}^*.$$

The perturbed solutions  $R^* + \Delta R$  and  $S^* + \Delta S$  are computed based on the method derived in [2] and using the software [3]. In our experiments we obtain  $\gamma_{\text{opt}} = 0.4191$ . The relative perturbation bounds for the solutions  $R^*$  and  $S^*$  of the LMIs (2)–(3) are obtained by the linear bounds (14) and (13), respectively.

The results obtained for different values of  $i$  are shown in the following table:

i	$\frac{\ \Delta s\ _2}{\ \text{vec}(S^*)\ _2}$	Граница (13)	$\frac{\ \Delta r\ _2}{\ \text{vec}(R^*)\ _2}$	Граница (14)
8	$0.1 \cdot 10^{-6}$	$0.5 \cdot 10^{-5}$	$0.7 \cdot 10^{-6}$	$6.3 \cdot 10^{-5}$
7	$0.1 \cdot 10^{-5}$	$0.5 \cdot 10^{-4}$	$0.7 \cdot 10^{-5}$	$6.3 \cdot 10^{-4}$
6	$0.1 \cdot 10^{-4}$	$0.5 \cdot 10^{-3}$	$0.7 \cdot 10^{-4}$	$6.3 \cdot 10^{-3}$
5	$0.1 \cdot 10^{-3}$	$0.5 \cdot 10^{-2}$	$0.7 \cdot 10^{-3}$	$6.3 \cdot 10^{-2}$
4	$0.1 \cdot 10^{-2}$	$0.5 \cdot 10^{-1}$	$0.7 \cdot 10^{-2}$	$6.3 \cdot 10^{-1}$

**5. Conclusions.** A complete local linear sensitivity analysis of the discrete LMI based on  $\mathcal{H}_\infty$  synthesis problem is done. Tight perturbation bounds, which are linear functions of the data perturbations, are obtained for the matrix inequalities determining the problem solution. A numerical example is presented which explicitly reveals the performance and applicability of the proposed approach to analyze the sensitivity of discrete LMI based  $\mathcal{H}_\infty$  synthesis problems.

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### ПЕРТУРБАЦИОННИ ГРАНИЦИ ЗА ДИСКРЕТНАТА $\mathcal{H}_\infty$ ЗАДАЧА ЗА СИНТЕЗ

**Андрей С. Йончев, Михаил М. Константинов, Петко Х. Петков**

В работата са намерени линейни пертурбационни граници за дискретната задача за синтеза, основана на линейни матрични неравенства (ЛМН). Направен е анализ на чувствителността на смутените матрични уравнения след въвеждане на подходящо избрани смутена дясна страна.