

## COVARIANT VECTOR DECOMPOSITION OF THREE-DIMENSIONAL ROTATIONS\*

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The main purpose of this paper is to provide an alternative representation for the generalized *Euler* decomposition (with respect to arbitrary axes) obtained in [1, 2] by means of vector parametrization of the *Lie* group  $SO(3)$ . The scalar (angular) parameters of the decomposition are explicitly written here as functions depending only on the contravariant components of the compound vector-parameter in the basis, determined by the three axes. We also consider the case of coplanar axes, in which the basis needs to be completed by a third vector and in particular, two-axes decompositions.

**1. Vector-parameters in the *Euler* decomposition.** Vector-parameters, also known as *Rodrigues'* or *Gibbs'* vectors, are naturally introduced via stereographic projection. For the rotation group in  $\mathbb{R}^3$  we consider the spin cover  $SU(2) \cong S^3 \rightarrow SO(3) \cong \mathbb{RP}^3$  and identify  $S^3$  with the set of the unit quaternions (cf. [4])

$$\zeta = (\zeta_0, \boldsymbol{\zeta}) = \zeta_0 + \zeta_1 \mathbf{i} + \zeta_2 \mathbf{j} + \zeta_3 \mathbf{k}, \quad |\zeta|^2 = \zeta \bar{\zeta} = 1, \quad \bar{\zeta} = (\zeta_0, -\boldsymbol{\zeta}), \quad \zeta_\alpha \in \mathbb{R}.$$

The corresponding group morphism is given by the adjoint action of  $S^3$  in its *Lie* algebra of skew-*Hermitian* matrices, in which we expand vectors  $\mathbf{x} \in \mathbb{R}^3 \rightarrow x_1 \mathbf{i} + x_2 \mathbf{j} + x_3 \mathbf{k} \in \mathfrak{su}(2)$ . The resulting  $SO(3)$  matrix transforming the *Cartesian* coordinates of  $\mathbf{x}$  has the form

$$(1) \quad \mathcal{R}(\zeta) = (\zeta_0^2 - \boldsymbol{\zeta}^2) \mathcal{I} + 2 \boldsymbol{\zeta} \otimes \boldsymbol{\zeta}^t + 2 \zeta_0 \boldsymbol{\zeta}^\times,$$

where  $\mathcal{I}$  and  $\boldsymbol{\zeta} \otimes \boldsymbol{\zeta}^t$  denote the identity and the tensor (dyadic) product in  $\mathbb{R}^3$  respectively, whereas  $\boldsymbol{\zeta}^\times$  is the skew-symmetric matrix, associated with the vector  $\boldsymbol{\zeta}$  via *Hodge* duality. The famous *Rodrigues'* rotation formula then follows directly with the substitution

$$\zeta_0 = \cos \frac{\varphi}{2}, \quad \boldsymbol{\zeta} = \sin \frac{\varphi}{2} \mathbf{n}, \quad (\mathbf{n}, \mathbf{n}) = 1.$$

On the other hand, we may choose to get rid of the unnecessary fourth coordinate by projecting  $\zeta \rightarrow \mathbf{c} = \frac{\boldsymbol{\zeta}}{\zeta_0} = \tan \left( \frac{\varphi}{2} \right) \mathbf{n}$  and thus obtain the entries of the rotation matrix (1) expressed as rational functions of the *vector-parameter*  $\mathbf{c}$  in the form

$$(2) \quad \mathcal{R}(\mathbf{c}) = \frac{(1 - \mathbf{c}^2) \mathcal{I} + 2 \mathbf{c} \otimes \mathbf{c}^t + 2 \mathbf{c}^\times}{1 + \mathbf{c}^2}.$$

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Quaternion multiplication then gives the composition law of vector-parameters as

$$(3) \quad \langle \mathbf{c}_2, \mathbf{c}_1 \rangle = \frac{\mathbf{c}_2 + \mathbf{c}_1 + \mathbf{c}_2 \times \mathbf{c}_1}{1 - (\mathbf{c}_2, \mathbf{c}_1)}, \quad \mathcal{R}(\mathbf{c}_2)\mathcal{R}(\mathbf{c}_1) = \mathcal{R}(\langle \mathbf{c}_2, \mathbf{c}_1 \rangle)$$

and in the case of three rotations  $\mathbf{c} = \langle \mathbf{c}_3, \mathbf{c}_2, \mathbf{c}_1 \rangle$  we have

$$(4) \quad \mathbf{c} = \frac{\mathbf{c}_3 + \mathbf{c}_2 + \mathbf{c}_1 + \mathbf{c}_3 \times \mathbf{c}_2 + \mathbf{c}_3 \times \mathbf{c}_1 + \mathbf{c}_2 \times \mathbf{c}_1 + (\mathbf{c}_3 \times \mathbf{c}_2) \times \mathbf{c}_1 - (\mathbf{c}_3, \mathbf{c}_2) \mathbf{c}_1}{1 - (\mathbf{c}_3, \mathbf{c}_2) - (\mathbf{c}_3, \mathbf{c}_1) - (\mathbf{c}_2, \mathbf{c}_1) + (\mathbf{c}_3, \mathbf{c}_2, \mathbf{c}_1)}.$$

It is not difficult to see that the operation is associative and constitutes a representation of  $\text{SO}(3)$ , since the identity and inverse elements are also well-defined by  $\langle \mathbf{c}, 0 \rangle = \langle 0, \mathbf{c} \rangle = \mathbf{c}$ ,  $\langle \mathbf{c}, -\mathbf{c} \rangle = 0$ . Among the advantages of this representation are more economical calculations, rational expressions for the matrix entries of  $\mathcal{R}(\mathbf{c})$  and a correct description of the topology of  $\text{SO}(3) \cong \mathbb{RP}^3$ . For applications in rigid body mechanics we refer to [3, 5].

As for the generalized *Euler* decompositions, we start with the much simpler two axes setting  $\mathcal{R}(\mathbf{c}) = \mathcal{R}(\mathbf{c}_2)\mathcal{R}(\mathbf{c}_1)$ , where  $\mathbf{c}_k = \tau_k \hat{\mathbf{c}}_k$  and  $\mathbf{c} = \tau \mathbf{n}$  ( $\hat{\mathbf{c}}_k^2 = \mathbf{n}^2 = 1$ ) are the corresponding vector-parameters. We also denote  $(\hat{\mathbf{c}}_j, \mathcal{R}(\mathbf{c}) \hat{\mathbf{c}}_k) = r_{jk}$  and  $(\hat{\mathbf{c}}_j, \hat{\mathbf{c}}_k) = g_{jk}$ . Taking an appropriate scalar product provides the necessary and sufficient condition for the existence of the above decomposition in the form  $r_{21} = g_{21}$ . Next, multiplying  $\mathbf{c} = \langle \mathbf{c}_2, \mathbf{c}_1 \rangle$  on the left by  $\mathbf{n}^\times$  and projecting along  $\hat{\mathbf{c}}_1$  and  $\hat{\mathbf{c}}_2$  respectively, we obtain

$$(5) \quad \tau_1 = \frac{\tilde{v}_3}{g_{12}v_1 - v_2}, \quad \tau_2 = \frac{\tilde{v}_3}{g_{12}v_2 - v_1},$$

where we make use of the notations

$$v_k = (\hat{\mathbf{c}}_k, \mathbf{n}), \quad \tilde{v}_1 = (\hat{\mathbf{c}}_2 \times \hat{\mathbf{c}}_3, \mathbf{n}), \quad \tilde{v}_2 = (\hat{\mathbf{c}}_3 \times \hat{\mathbf{c}}_1, \mathbf{n}), \quad \tilde{v}_3 = (\hat{\mathbf{c}}_1 \times \hat{\mathbf{c}}_2, \mathbf{n}).$$

Note that vanishing denominators in the above expressions are related to *half-turns*, i.e., rotations by a straight angle. In particular, if  $\mathbf{n} \perp \hat{\mathbf{c}}_{1,2}$  ( $v_1 = v_2 = 0$ ), we have a decomposition into a pair of reflections, which is a well-known result in elementary geometry.

In the case of three axes  $\mathcal{R}(\mathbf{c}) = \mathcal{R}(\mathbf{c}_3)\mathcal{R}(\mathbf{c}_2)\mathcal{R}(\mathbf{c}_1)$ , such that  $\hat{\mathbf{c}}_2$  cannot be parallel to  $\hat{\mathbf{c}}_1$  or  $\hat{\mathbf{c}}_3$ , we use the scalar product  $(\hat{\mathbf{c}}_3, \mathcal{R}(\mathbf{c}) \hat{\mathbf{c}}_1) = (\hat{\mathbf{c}}_3, \mathcal{R}(\tau_2 \hat{\mathbf{c}}_2) \hat{\mathbf{c}}_1)$  to obtain

$$(r_{31} + g_{31} - 2g_{12}g_{23})\tau_2^2 + 2\omega\tau_2 + r_{31} - g_{31} = 0, \quad \omega = (\hat{\mathbf{c}}_1, \hat{\mathbf{c}}_2 \times \hat{\mathbf{c}}_3).$$

The above quadratic equation has real roots given by

$$(6) \quad \tau_2^\pm = \frac{-\omega \pm \sqrt{\Delta}}{r_{31} + g_{31} - 2g_{12}g_{23}}$$

as long as its discriminant is non-negative

$$(7) \quad \Delta = \begin{vmatrix} 1 & g_{12} & r_{31} \\ g_{21} & 1 & g_{23} \\ r_{31} & g_{32} & 1 \end{vmatrix} \geq 0$$

which plays the role of a necessary and sufficient condition for the existence of the decomposition. In order to find the remaining two scalar parameters, we use the composition

$$\mathbf{c}_1 = \langle -\mathbf{c}_2, -\mathbf{c}_3, \mathbf{c} \rangle, \quad \mathbf{c}_2 = \langle -\mathbf{c}_3, \mathbf{c}, -\mathbf{c}_1 \rangle, \quad \mathbf{c}_3 = \langle \mathbf{c}, -\mathbf{c}_1, -\mathbf{c}_2 \rangle.$$

Namely, multiplying by  $\hat{\mathbf{c}}_k^\times$  on the left and projecting over  $\mathbf{n}$ , we obtain the linear-fractional relations between  $\tau_k$ , which yield the solutions for the generic case in the form

$$(8) \quad \begin{aligned} \tau_1^\pm &= \frac{g_{32} - r_{32}}{(g_{32} + r_{32})\tau v_1 - (g_{31} + r_{31})\tau v_2 + (r_{31} - g_{31})/\tau_2^\pm} \\ \tau_3^\pm &= \frac{g_{21} - r_{21}}{(g_{21} + r_{21})\tau v_3 - (g_{31} + r_{31})\tau v_2 + (r_{31} - g_{31})/\tau_2^\pm} \end{aligned}$$

while in the symmetric one we consider the limit  $\tau \rightarrow \infty$  and thus obtain

$$(9) \quad \tau_1^\pm = \frac{g_{23} - v_2 v_3}{v_1 \tilde{v}_1 + v_2 \tilde{v}_2 + (v_1 v_3 - g_{13})/\tau_2^\pm}, \quad \tau_3^\pm = \frac{g_{12} - v_1 v_2}{v_2 \tilde{v}_2 + v_3 \tilde{v}_3 + (v_1 v_3 - g_{13})/\tau_2^\pm}.$$

In the three axes setting we may also have degenerate solutions, related to a singularity of the map  $\mathbb{R}\mathbb{P}^3 \rightarrow \mathbb{T}^3$ , known as *gimbal lock*, which is given by the condition

$$(10) \quad \hat{\mathbf{c}}_3 = \pm \mathcal{R}(\mathbf{c}) \hat{\mathbf{c}}_1.$$

In that case the parameters  $\tau_1$  and  $\tau_3$  cannot be determined independently. Instead, we have the effective two-axes decomposition  $\mathcal{R}(\mathbf{c}) = \mathcal{R}(\tau_2 \hat{\mathbf{c}}_2) \mathcal{R}(\tilde{\tau}_1 \hat{\mathbf{c}}_1)$ , where the solutions

$$(11) \quad \tilde{\tau}_1 = \frac{\tau_1 \pm \tau_3}{1 \mp \tau_1 \tau_3} = \frac{\tilde{v}_3}{g_{12} v_1 - v_2}, \quad \tau_2 = \frac{\tilde{v}_3}{g_{12} v_2 - v_1}$$

form an one-parameter set, expressed in terms of the generalized *Euler* angles as

$$\varphi_1 \pm \varphi_3 = 2 \arctan \left( \frac{\tilde{v}_3}{g_{12} v_1 - v_2} \right), \quad \varphi_2 = 2 \arctan \left( \frac{\tilde{v}_3}{g_{12} v_2 - v_1} \right).$$

**2. Covariant form of the solutions.** First, we consider the simpler case of two axes  $\mathbf{c} = \langle \tau_2 \hat{\mathbf{c}}_2, \tau_1 \hat{\mathbf{c}}_1 \rangle$ , in which it is necessary to complete the basis with a third vector

$$(12) \quad \mathbf{c} = \xi_1 \hat{\mathbf{c}}_1 + \xi_2 \hat{\mathbf{c}}_2 + \xi_3 \hat{\mathbf{c}}_1 \times \hat{\mathbf{c}}_2.$$

If we denote the adjoint matrix of  $g$  with  $\gamma$ , we have  $|\hat{\mathbf{c}}_1 \times \hat{\mathbf{c}}_2|^2 = 1 - g_{12}^2 = \gamma^{33}$ . Note that in formula (5) we use the covariant components of  $\mathbf{c}$  in the same basis

$$(13) \quad \tau v_1 = \xi_1 + g_{12} \xi_2, \quad \tau v_2 = \xi_2 + g_{12} \xi_1, \quad \tau \tilde{v}_3 = \gamma^{33} \xi_3.$$

Thus, by direct substitution, we obtain the decomposability condition  $r_{21} = g_{21}$  as

$$(14) \quad \xi_1 \xi_2 + (1 - g_{12} \xi_3) \xi_3 = 0$$

and the solutions themselves are given by the expressions

$$(15) \quad \tau_1 = -\xi_3/\xi_2, \quad \tau_2 = -\xi_3/\xi_1.$$

One peculiar symmetry becomes apparent from the above formula, namely  $\tau_1 \xi_2 - \tau_2 \xi_1 = 0$ .

In the three axes setting we first consider the case, in which  $\{\hat{\mathbf{c}}_k\}$  constitutes a basis

$$\mathbf{c} = \xi_1 \hat{\mathbf{c}}_1 + \xi_2 \hat{\mathbf{c}}_2 + \xi_3 \hat{\mathbf{c}}_3 = \langle \tau_3 \hat{\mathbf{c}}_3, \tau_2 \hat{\mathbf{c}}_2, \tau_1 \hat{\mathbf{c}}_1 \rangle.$$

We substitute the matrix entries  $r_{ij}$ , calculated according to (2) in the solutions (6), (8)

and use the inverse metric tensor  $g^{-1} = \omega^{-2}\gamma$  for lifting the indices of  $\mathbf{c}$ . Thus, we obtain

$$\tau_2^\pm = \frac{-\omega \pm \sqrt{\omega^2 - \sigma^2 + 2\gamma^{13}\sigma}}{\sigma - 2\gamma^{13}}, \quad \sigma = 2\frac{\gamma^{13}\xi_2^2 - \gamma^{23}\xi_1\xi_2 - \gamma^{12}\xi_2\xi_3 + \gamma^{22}\xi_1\xi_3 - \omega\xi_2}{\xi_1^2 + \xi_2^2 + \xi_3^2 + 2g_{12}\xi_1\xi_2 + 2g_{23}\xi_2\xi_3 + 2g_{13}\xi_1\xi_3}$$

for the middle parameter and for the other two

$$(16) \quad \begin{aligned} \tau_1^\pm &= \frac{\gamma^{13}\xi_1\xi_2 + \gamma^{12}\xi_1\xi_3 - \gamma^{11}\xi_2\xi_3 - \gamma^{23}\xi_1^2 - \omega\xi_1}{\omega(\xi_1^2 + \xi_2^2 + 2g_{12}\xi_1\xi_2 + g_{13}\xi_1\xi_3 + g_{23}\xi_2\xi_3) - \gamma^{23}\xi_1 + \gamma^{13}\xi_2 + \kappa_2/\tau_2^\pm} \\ \tau_3^\pm &= \frac{\gamma^{13}\xi_2\xi_3 + \gamma^{23}\xi_1\xi_3 - \gamma^{33}\xi_1\xi_2 - \gamma^{12}\xi_3^2 - \omega\xi_3}{\omega(\xi_2^2 + \xi_3^2 + g_{12}\xi_1\xi_2 + g_{13}\xi_1\xi_3 + 2g_{23}\xi_2\xi_3) + \gamma^{13}\xi_2 - \gamma^{12}\xi_3 + \kappa_2/\tau_2^\pm} \end{aligned}$$

respectively, in which we use the notation  $\kappa_2 = \gamma^{13}\xi_2^2 - \gamma^{23}\xi_1\xi_2 - \gamma^{12}\xi_2\xi_3 + \gamma^{22}\xi_1\xi_3 - \omega\xi_2$ .

In the case  $\omega = 0$  we use expansion in the basis (12) and the explicit relations (13) between the covariant and contravariant components of  $\mathbf{c}$  in order to obtain

$$(17) \quad \tau_2^\pm = \pm\sqrt{\frac{\dot{\sigma}}{2\gamma^{13} - \dot{\sigma}}}, \quad \dot{\sigma} = 2\frac{\gamma^{13}\xi_2^2 - \gamma^{23}(\xi_1\xi_2 + \xi_3) - g_{13}\gamma^{33}\xi_3^2}{1 + \xi_1^2 + \xi_2^2 + \gamma^{33}\xi_3^2 + 2g_{12}\xi_1\xi_2}.$$

Denoting  $\hat{\kappa}_2 = \gamma^{13}\xi_2^2 - \gamma^{23}(\xi_1\xi_2 + \xi_3) - g_{13}\gamma^{33}\xi_3^2$ , we have for  $\tau_{1,3}$  the expressions

$$(18) \quad \begin{aligned} \tau_1^\pm &= \frac{\gamma^{13}(\xi_1\xi_2 - \xi_3) - \gamma^{23}\xi_1^2 + g_{23}\gamma^{33}\xi_3^2}{(\gamma^{13} + g_{12}\gamma^{23})\xi_1\xi_3 + (\gamma^{23} + g_{12}\gamma^{13})\xi_2\xi_3 + \gamma^{13}\xi_2 - \gamma^{23}\xi_1 + \hat{\kappa}_2/\tau_2^\pm} \\ \tau_3^\pm &= \frac{g_{12}\xi_3^2 - \gamma^{33}(\xi_1\xi_2 + \xi_3)}{(g_{12}\gamma^{23} + g_{13}\gamma^{33})\xi_1\xi_3 + (\gamma^{23} + g_{23}\gamma^{33})\xi_2\xi_3 + \gamma^{13}\xi_2 + \hat{\kappa}_2/\tau_2^\pm}. \end{aligned}$$

If the compound rotation is symmetric, i.e.,  $\varphi = \pi$  and  $\mathcal{R}(\mathbf{c}) = \mathcal{O}(\mathbf{n}) = 2\mathbf{n} \otimes \mathbf{n}^t - \mathcal{I}$ , considering the limit  $\tau \rightarrow \infty$  in the solutions we substitute the coordinates  $\xi_k$  with the contravariant components  $\eta_k$  in the expansion of the unit vector  $\mathbf{n}$  ( $\xi_k = \tau\eta_k$ ) dropping all linear and constant terms in the expressions. For example, in the case  $\omega = 0$  we have

$$(19) \quad \begin{aligned} \tau_1^\pm &= \frac{\gamma^{13}\eta_1\eta_2 - \gamma^{23}\eta_1^2 + g_{23}\gamma^{33}\eta_3^2}{(\gamma^{13} + g_{12}\gamma^{23})\eta_1\eta_3 + (\gamma^{23} + g_{12}\gamma^{13})\eta_2\eta_3 + (\gamma^{13}\eta_2^2 - \gamma^{23}\eta_1\eta_2 - g_{13}\gamma^{33}\eta_3^2)/\tau_2^\pm} \\ \tau_3^\pm &= \frac{g_{12}\eta_3^2 - \gamma^{33}\eta_1\eta_2}{(g_{12}\gamma^{23} + g_{13}\gamma^{33})\eta_1\eta_3 + (\gamma^{23} + g_{23}\gamma^{33})\eta_2\eta_3 + (\gamma^{13}\eta_2^2 - \gamma^{23}\eta_1\eta_2 - g_{13}\gamma^{33}\eta_3^2)/\tau_2^\pm} \end{aligned}$$

where

$$(20) \quad \tau_2^\pm = \pm\sqrt{\frac{\dot{\sigma}}{2\gamma^{13} - \dot{\sigma}}}, \quad \dot{\sigma} = 2\frac{\gamma^{13}\eta_2^2 - \gamma^{23}\eta_1\eta_2 - g_{13}\gamma^{33}\eta_3^2}{\eta_1^2 + \eta_2^2 + \gamma^{33}\eta_3^2 + 2g_{12}\eta_1\eta_2}.$$

The case  $\omega \neq 0$  is treated similarly and so is the decomposition with respect to two axes.

As for the degenerate case (10), if  $\omega = 0$  we may use the result obtained in the two axes setting combined with (11) in order to express

$$(21) \quad \tilde{\tau}_1 = \frac{\tau_1 \pm \tau_3}{1 \mp \tau_1\tau_3} = -\frac{\xi_3}{\xi_2}, \quad \tau_2 = -\frac{\xi_3}{\xi_1}.$$

If  $\omega \neq 0$  on the other hand, the solutions are given by

$$(22) \quad \tilde{\tau}_1 = \frac{\tau_1 \pm \tau_3}{1 \mp \tau_1 \tau_3} = \frac{\omega \xi_3}{\gamma^{23} \xi_3 - \gamma^{33} \xi_1}, \quad \tau_2 = \frac{\omega \xi_3}{\gamma^{13} \xi_3 - \gamma^{33} \xi_1}.$$

In both cases we may use  $\eta_k$  instead of  $\xi_k$  so that the expressions are valid when  $\tau \rightarrow \infty$ .

If we need to express  $\xi_k$  on the other hand, it is straightforward to use the composition law (4) and then take the correct scalar products. Thus, in the case  $\omega \neq 0$  we obtain

$$(23) \quad \begin{aligned} \xi_1 &= \frac{(1 - g_{23} \tau_2 \tau_3) \tau_1 + \omega^{-1} (\gamma^{12} \tau_1 \tau_3 - \gamma^{13} \tau_1 \tau_2 - \gamma^{11} \tau_2 \tau_3)}{1 - g_{12} \tau_1 \tau_2 - g_{13} \tau_1 \tau_3 - g_{23} \tau_2 \tau_3 + \omega \tau_1 \tau_2 \tau_3} \\ \xi_2 &= \frac{(1 + g_{13} \tau_1 \tau_3) \tau_2 + \omega^{-1} (\gamma^{22} \tau_1 \tau_3 - \gamma^{12} \tau_2 \tau_3 - \gamma^{23} \tau_1 \tau_2)}{1 - g_{12} \tau_1 \tau_2 - g_{13} \tau_1 \tau_3 - g_{23} \tau_2 \tau_3 + \omega \tau_1 \tau_2 \tau_3} \\ \xi_3 &= \frac{(1 - g_{12} \tau_1 \tau_2) \tau_3 + \omega^{-1} (\gamma^{23} \tau_1 \tau_3 - \gamma^{13} \tau_2 \tau_3 - \gamma^{33} \tau_1 \tau_2)}{1 - g_{12} \tau_1 \tau_2 - g_{13} \tau_1 \tau_3 - g_{23} \tau_2 \tau_3 + \omega \tau_1 \tau_2 \tau_3}. \end{aligned}$$

For  $\omega = 0$  the corresponding result is

$$\begin{aligned} \dot{\xi}_1 &= \frac{(1 - g_{23} \tau_2 \tau_3) \tau_1 - \gamma^{13} (1 - g_{12} \tau_1 \tau_2) \tau_3 / \gamma^{33}}{1 - g_{12} \tau_1 \tau_2 - g_{13} \tau_1 \tau_3 - g_{23} \tau_2 \tau_3} \\ \dot{\xi}_2 &= \frac{(1 + g_{13} \tau_1 \tau_3) \tau_2 - \gamma^{23} (1 - g_{12} \tau_1 \tau_2) \tau_3 / \gamma^{33}}{1 - g_{12} \tau_1 \tau_2 - g_{13} \tau_1 \tau_3 - g_{23} \tau_2 \tau_3}, \quad \dot{\xi}_3 = \frac{\gamma^{23} \tau_1 \tau_3 / \gamma^{33} - \gamma^{13} \tau_2 \tau_3 / \gamma^{33} - \tau_1 \tau_2}{1 - g_{12} \tau_1 \tau_2 - g_{13} \tau_1 \tau_3 - g_{23} \tau_2 \tau_3}. \end{aligned}$$

Likewise, in the case of two axes we have a linear system for  $\xi_{1,2}$  with solutions, given by

$$(24) \quad \xi_1 = \frac{\tau_1}{1 - g_{12} \tau_1 \tau_2}, \quad \xi_2 = \frac{\tau_2}{1 - g_{12} \tau_1 \tau_2}.$$

Since the above expressions are rational in terms of the parameters  $\tau_j$ , if any of these diverges, i.e.,  $\varphi_k = \pi$ , we can still obtain the correct formulae, applying *l'Hôpital's* rule.

Similar expressions hold for the relations between the scalar parameters and the covariant components of  $\mathbf{c}$  in the corresponding basis. However, these are almost straightforward to write considering the results obtained in [1, 2]. Another possible generalization involves the hyperbolic case, i.e., the three-dimensional *Lorentz* group  $\text{SO}(2, 1)$ , which can be treated in an analogous way. Some of the advantages of this new representation for the numerous applications of the generalized Euler decomposition (cf. [3, 4, 5]) are quite obvious. The explicit dependence only on the contravariant components allows, apart from its purely geometric merits, for straightforward differentiation, as well as for obtaining the decomposition in a rotated frame from one that has been given.

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## КОВАРИАНТНО РАЗЛАГАНЕ НА ТРИМЕРНИ РОТАЦИИ

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В тази статия предлагаме алтернативно представяне на решенията, получени преди това в [1, 2] за обобщеното разлагане на *Euler* (около три произволни оси) чрез векторна параметризация на групата  $SO(3)$ . Скаларните (ъглови) параметри в разлагането са представени като явни функции, зависещи само от контравариантните компоненти на вектор-параметъра на композитната ротация в базиса, определен от трите оси в разлагането. Отделно сме разгледали случаите, в които осите са компланарни и базисът следва да бъде допълнен, и в частност разлагането на две въртения.